

Linear Systems and Signals

An application: the inverted pendulum

Anand D. Sarwate

Department of Electrical and Computer Engineering
Rutgers, The State University of New Jersey

2020



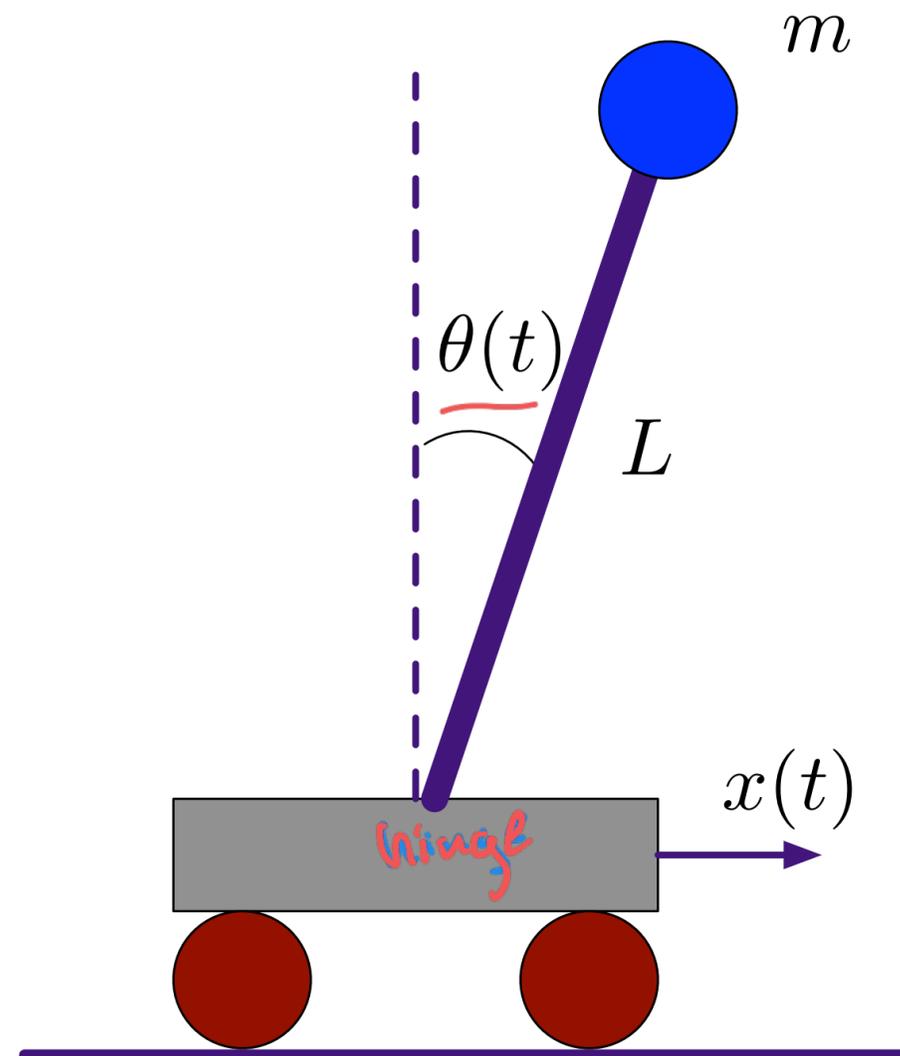
Learning objectives

The learning objectives for this section are:

- understand how to model a physical system as an LTI system
- apply feedback control to stabilize a real-world system

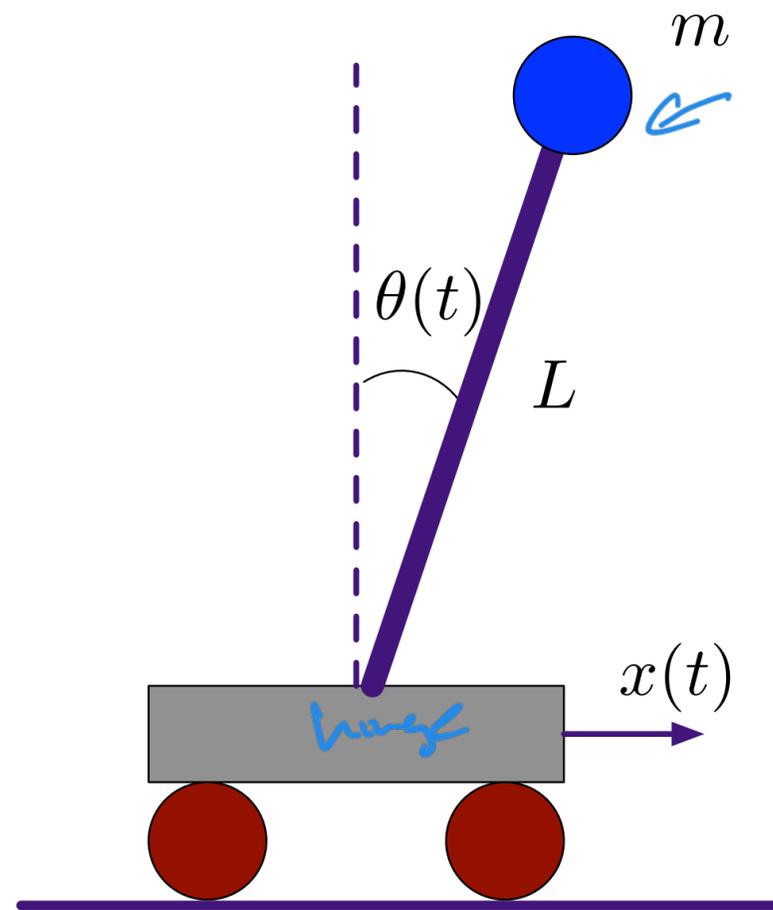


The inverted pendulum



The inverted pendulum is a commonly-studied example for feedback control: a mass is balanced on a rod connected to a cart. We want to move the cart back and forth to keep the mass m vertical.

The physical set up



We'll simplify the model to assume the cart and rod are massless and the connector between the rod and cart is frictionless.

- $x(t)$ is the position of cart
- $\theta(t)$ is the angular displacement of the rod
- L is the length of the rod (important for torque)

Balancing torques

We have look at the different torques acting on the mass m .

- $m(L \sin(\theta(t)))g$ is due to gravity on the mass, where $g = 9.8 \frac{\text{m}}{\text{sec}^2}$.
- $-m(L \cos(\theta(t))) \frac{d^2}{dt^2} x(t)$ from the cart being displaced by $x(t)$.
- $mL^2 \frac{d^2}{dt^2} \theta(t)$ is from angular acceleration (moment of inertia mL^2).

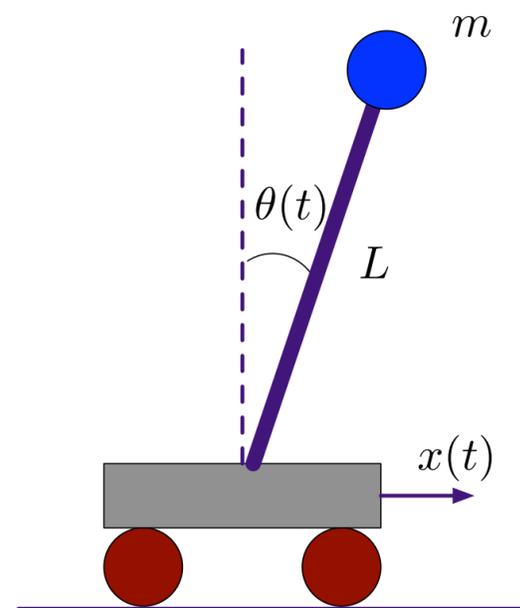
We have to set the angular acceleration torque equal to the sum of the two torques:

$$mL^2 \frac{d^2}{dt^2} \theta(t) = m(L \sin(\theta(t)))g - m(L \cos(\theta(t))) \frac{d^2}{dt^2} x(t) \quad (1)$$

This is *not* an LCCDE.



Approximation for small displacements



If θ is too big we have no hope of stabilizing the system, so let's assume $\theta(t) \ll 1$ remains small. In that case we can use a Taylor series to approximate the sine and cosine:

$$\sin(\theta(t)) = \theta(t) - \frac{\theta(t)^3}{3!} + \dots \approx \theta(t)$$

$$\cos(\theta(t)) = 1 - \frac{\theta(t)^2}{2!} + \dots \approx 1$$

Linearization of the functions/system (2)

Linearizing the differential equation

So this simplifies our differential equation to an LCCDE:

$$mL^2 \frac{d^2}{dt^2} \theta(t) = m(L \sin(\theta(t)))g - m(L \cos(\theta(t))) \frac{d^2}{dt^2} x(t) \quad (4)$$

$$mL^2 \frac{d^2}{dt^2} \theta(t) = mLg\theta(t) - mL \frac{d^2}{dt^2} x(t). \quad (5)$$

Now we can divide by mL^2 :

$$\frac{d^2}{dt^2} \theta(t) = \frac{g}{L} \theta(t) - \frac{1}{L} \frac{d^2}{dt^2} x(t). \quad (6)$$

Taking Laplace transforms:

$$G(s) = \frac{\Theta(s)}{X(s)} = -\frac{s^2/L}{s^2 - g/L}. \quad (7)$$

open loop *Plant*



Pole-zero analysis

The transfer function is

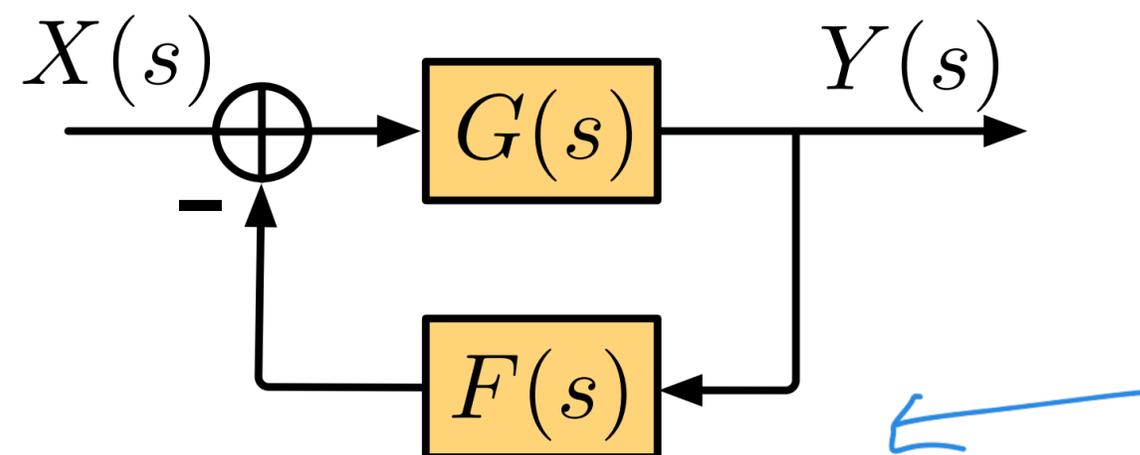
$$G(s) = -\frac{s^2/L}{s^2 - g/L} = -\frac{s^2}{Ls^2 - g}. \quad (8)$$

Poles are at $\pm\sqrt{g/L}$. Since this physical system is causal, the ROC is $\Re\{s\} > \sqrt{g/L}$ which does not contain the imaginary axis so the system is unstable.

- We can compute the output of the system to different signals $x(t)$ and see that the system output will blow up.
- Suppose we have a sensor that can measure $\theta(t)$. Can we use feedback to stabilize this system?



PI control



The plant is $G(s) = -\frac{s^2/L}{s^2-g/L}$. Using closed-loop feedback control we can try to stabilize the system. Let's try proportional-integral (PI) control:

$$F(s) = K_p + K_i \frac{1}{s} \quad (9)$$

*try to show
P/PD control
don't
work*

Then we have for the closed-loop system

$$H(s) = \frac{G(s)}{1 + \underline{F(s)G(s)}} = \frac{-\frac{s^2}{Ls^2-g}}{1 - \underline{(K_p + K_i/s)} \frac{s^2}{Ls^2-g}} \quad (10)$$



Finding the feedback system

The closed-loop system is

$$H(s) = \frac{-\frac{s^2}{Ls^2 - g}}{1 - (K_p + K_i/s)\frac{s^2}{Ls^2 - g}} \quad (11)$$

$$= \frac{-s^2}{\underbrace{(L - K_p)}_{\text{blue underline}} s^2 - \underbrace{K_i s}_{\text{blue underline}} - \underbrace{g}_{\text{blue underline}}} \quad (12)$$

We have two zeros at 0 and two poles: with two parameters to control the system we can move the poles to many different locations. To get a stable system, let's first set $\underline{K_p = L + \alpha}$, so

$$H(s) = \frac{s^2}{\underline{\alpha s^2} + K_i s + g} \quad (13)$$

Now we can find the pole locations and move them around.



Pole locations: root locus

Starting with

$$H(s) = \frac{s^2}{\alpha s^2 + K_i s + g} \quad (14)$$

closed loop system

we have poles at

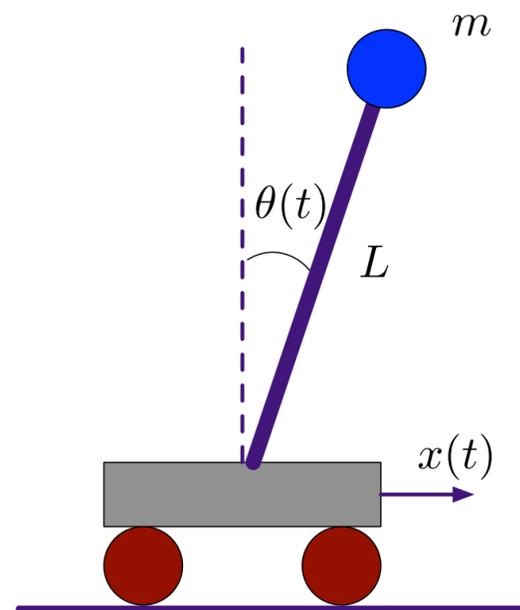
$$s = \frac{-K_i \pm \sqrt{K_i^2 - 4\alpha g}}{2\alpha} \quad (15)$$

root locus

We can see where these move numerically. We can consider the “*critically damped*” case where the poles are the same, in which case we have $K_i^2 = 4\alpha g$. For example, if $\alpha = 0.5$ then we can set $K_i = \sqrt{2g}$.



Recap



We started with a simplified physical system that we wanted to analyze.

- Use the physics to write down a differential equation describing the relationship between signals.
- Linearize the model by making appropriate assumptions about parameters/signal values.
- Generate the Laplace transform for the open-loop system.
- Close the loop by applying feedback control.
- Find parameters that can stabilize the closed-loop system.

More questions

We can write down a lot of different physical systems using RLC circuits or spring-mass-damper mechanical systems. These will lead to Laplace transforms that we can then analyze and apply feedback for stabilization.

Problem

Try proportional (P) and proportional-derivative (PD) control on the inverted pendulum and convince yourself that these policies cannot stabilize the system.

Try a PID control system and see how this might change how you can move the poles and zeros around. Does the added derivative control help that much?

$$F(s) = K_p + \underline{K_d s} + \underline{K_i \frac{1}{s}}$$

