

# Linear Systems and Signals

An application: the inverted pendulum

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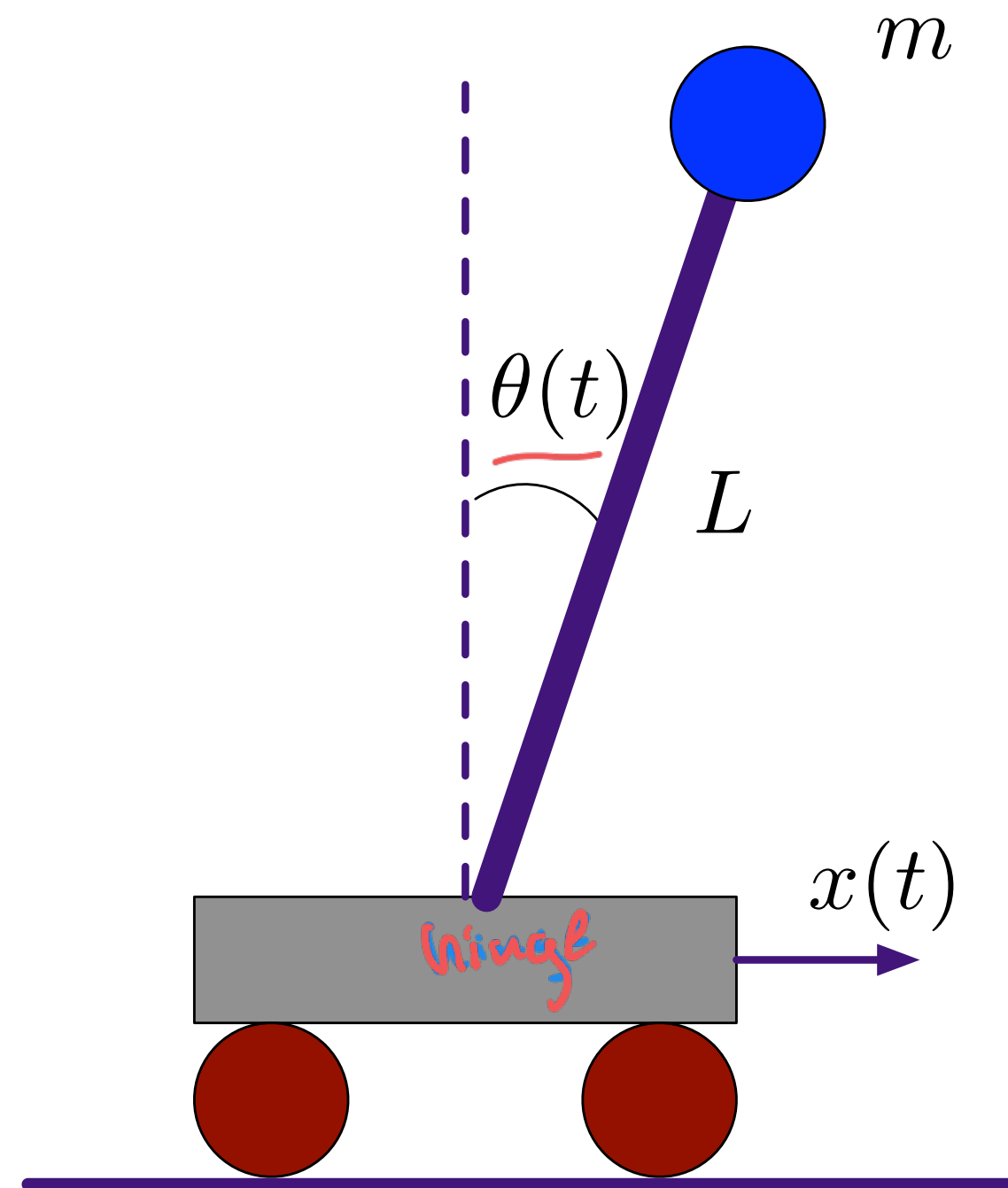
# Learning objectives

The learning objectives for this section are:

- understand how to model a physical system as an LTI system
- apply feedback control to stabilize a real-world system

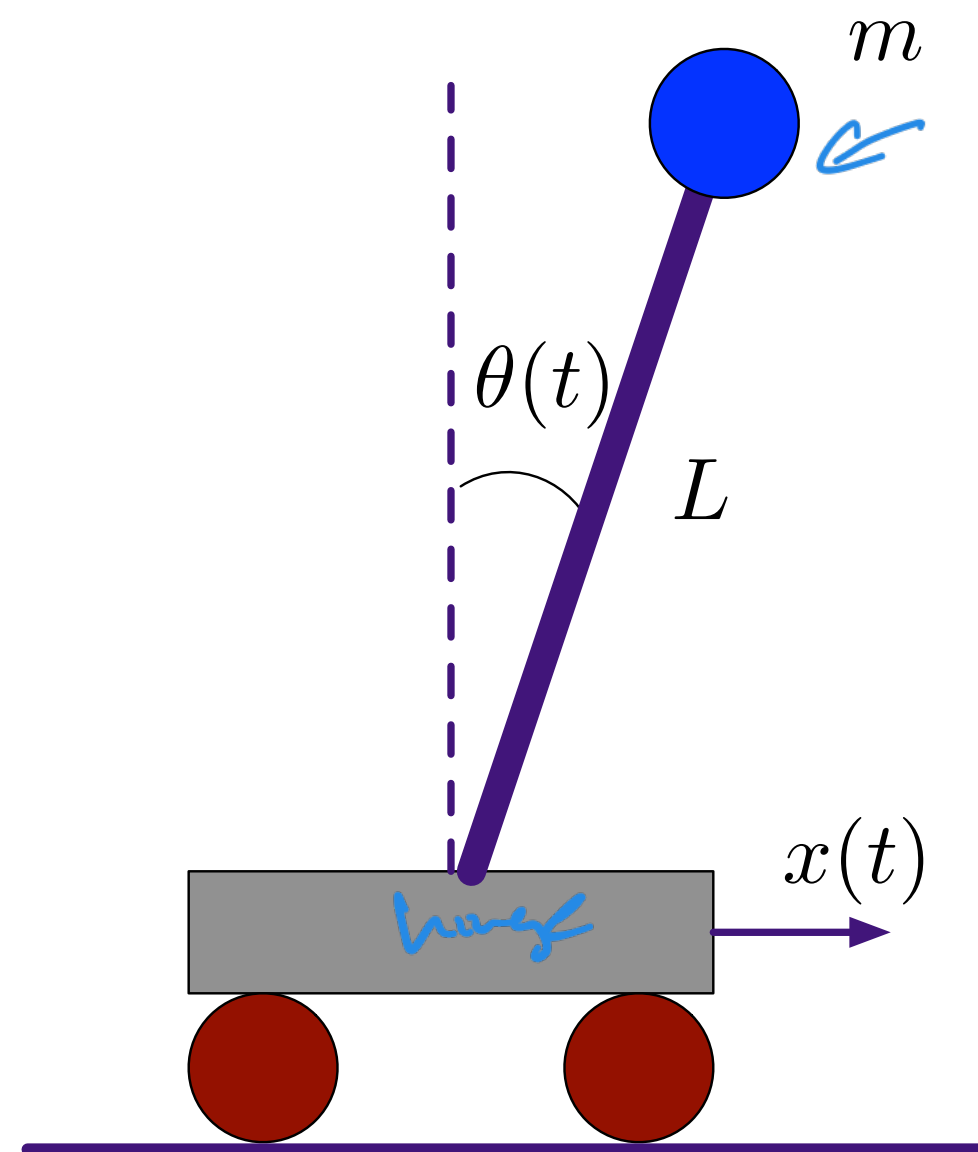


# The inverted pendulum



The inverted pendulum is a commonly-studied example for feedback control: a mass is balanced on a rod connected to a cart. We want to move the cart back and forth to keep the mass  $m$  vertical.

# The physical set up



We'll simplify the model to assume the cart and rod are massless and the connector between the rod and cart is frictionless.

- $x(t)$  is the position of cart
- $\theta(t)$  is the angular displacement of the rod
- $L$  is the length of the rod (important for torque)

# Balancing torques

We have look at the different torques acting on the mass  $m$ .

- $m(L \sin(\theta(t)))g$  is due to gravity on the mass, where  $g = 9.8 \frac{\text{m}}{\text{sec}^2}$ .
- $-m(L \cos(\theta(t))) \frac{d^2}{dt^2} x(t)$  from the cart being displaced by  $x(t)$ .
- $mL^2 \frac{d^2}{dt^2} \theta(t)$  is from angular acceleration (moment of inertia  $mL^2$ ).

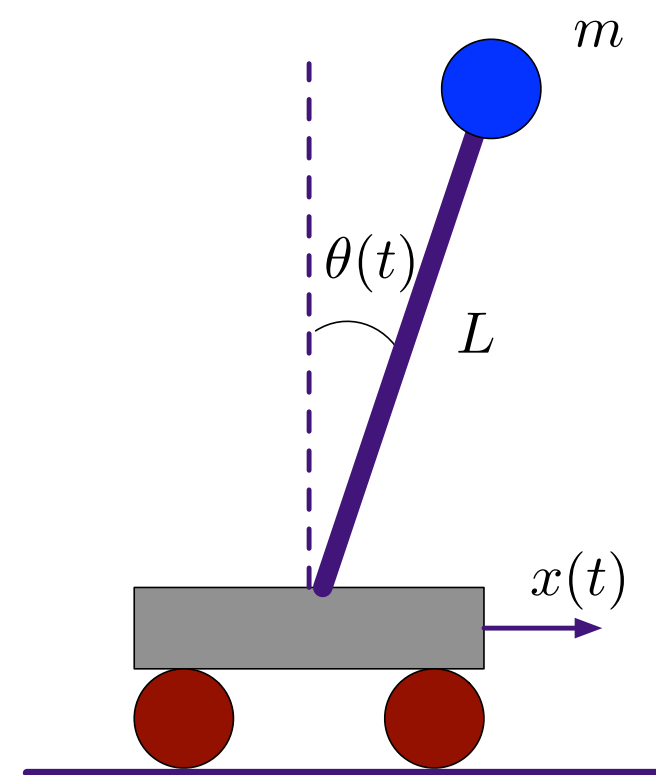
We have to set the angular acceleration torque equal to the sum of the two torques:

$$mL^2 \frac{d^2}{dt^2} \theta(t) = m(L \sin(\theta(t)))g - m(L \cos(\theta(t))) \frac{d^2}{dt^2} x(t) \quad (1)$$

This is *not* an LCCDE.



# Approximation for small displacements



If  $\theta$  is too big we have no hope of stabilizing the system, so let's assume  $\theta(t) \ll 1$  remains small. In that case we can use a Taylor series to approximate the sine and cosine:

$$\sin(\theta(t)) = \theta(t) - \frac{\theta(t)^3}{3!} + \dots \approx \theta(t) \quad (2)$$

*linearization of the functions / system*

$$\cos(\theta(t)) = 1 - \frac{\theta(t)^2}{2!} + \dots \approx 1 \quad (3)$$

# Linearizing the differential equation

So this simplifies our differential equation to an LCCDE:

$$mL^2 \frac{d^2}{dt^2} \theta(t) = m(L \sin(\theta(t)))g - m(L \cos(\theta(t))) \frac{d^2}{dt^2} x(t) \quad (4)$$

$$mL^2 \frac{d^2}{dt^2} \theta(t) = mLg\theta(t) - mL \frac{d^2}{dt^2} x(t). \quad (5)$$

Now we can divide by  $mL^2$ :

$$\frac{d^2}{dt^2} \theta(t) = \frac{g}{L} \theta(t) - \frac{1}{L} \frac{d^2}{dt^2} x(t). \quad (6)$$

Taking Laplace transforms:

open loop plant

$$G(s) = \frac{\Theta(s)}{X(s)} = -\frac{s^2/L}{s^2 - g/L}. \quad (7)$$



# Pole-zero analysis

The transfer function is

$$G(s) = -\frac{s^2/L}{s^2 - \underline{g/L}} = -\frac{s^2}{Ls^2 - g}. \quad (8)$$

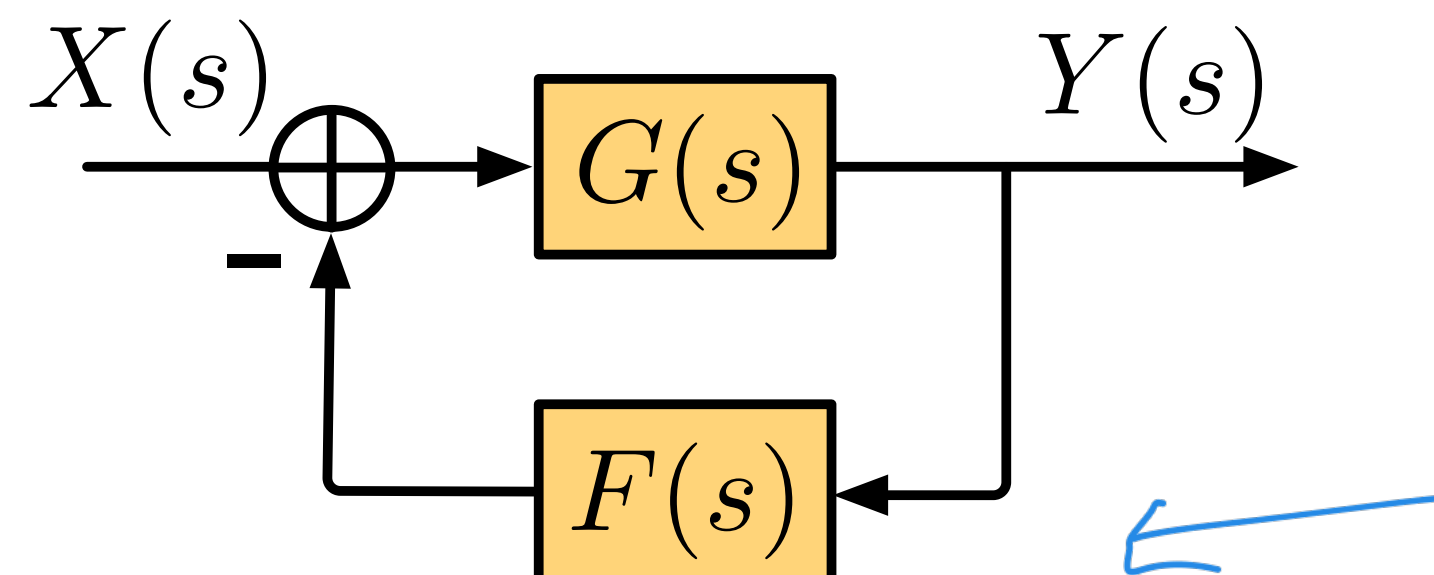
Poles are at  $\pm\sqrt{g/L}$ . Since this physical system is causal, the ROC is  $\Re\{s\} > \sqrt{g/L}$  which does not contain the imaginary axis so the system is unstable.

- We can compute the output of the system to different signals  $x(t)$  and see that the system output will blow up.
- Suppose we have a sensor that can measure  $\theta(t)$ . Can we use feedback to stabilize this system?





# PI control



The plant is  $G(s) = -\frac{s^2/L}{s^2 - g/L}$ . Using closed-loop feedback control we can try to stabilize the system. Let's try proportional-integral (PI) control:

$$F(s) = K_p + K_i \frac{1}{s} \quad (9)$$

*try to show P/PD control don't work*

Then we have for the closed-loop system

$$H(s) = \frac{G(s)}{1 + \underline{F(s)G(s)}} = \frac{-\frac{s^2}{Ls^2 - g}}{1 - \underline{(K_p + K_i/s) \frac{s^2}{Ls^2 - g}}} \quad (10)$$

# Finding the feedback system

The closed-loop system is

$$H(s) = \frac{-\frac{s^2}{Ls^2 - g}}{1 - (K_p + K_i/s)\frac{s^2}{Ls^2 - g}} \quad (11)$$

$$= \frac{-s^2}{(\underline{L - K_p})s^2 - \underline{K_i s} - \underline{g}} \quad (12)$$

We have two zeros at 0 and two poles: with two parameters to control the system we can move the poles to many different locations. To get a stable system, let's first set  $K_p = L + \alpha$ , so

$$H(s) = \frac{s^2}{\underline{\alpha s^2} + K_i s + g} \quad (13)$$

Now we can find the pole locations and move them around.



# Pole locations: root locus

Starting with

$$H(s) = \frac{s^2}{\alpha s^2 + K_i s + g} \quad (14)$$

closed loop system

we have poles at

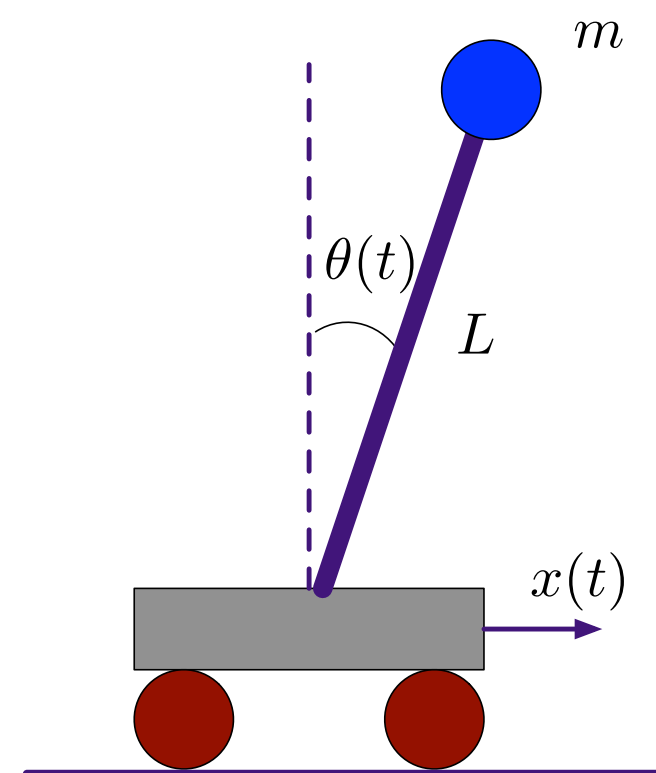
$$s = \frac{-K_i \pm \sqrt{K_i^2 - 4\alpha g}}{2\alpha} \quad (15)$$

root locus

We can see where these move numerically. We can consider the “critically damped” case where the poles are the same, in which case we have  $K_i^2 = 4\alpha g$ . For example, if  $\alpha = 0.5$  then we can set  $K_i = \sqrt{2g}$ .



# Recap



We started with a simplified physical system that we wanted to analyze.

- Use the physics to write down a differential equation describing the relationship between signals.
- Linearize the model by making appropriate assumptions about parameters/signal values.
- Generate the Laplace transform for the open-loop system.
- Close the loop by applying feedback control.
- Find parameters that can stabilize the closed-loop system.

# More questions

We can write down a lot of different physical systems using RLC circuits or spring-mass-damper mechanical systems. These will lead to Laplace transforms that we can then analyze and apply feedback for stabilization.

## Problem

*Try proportional (P) and proportional-derivative (PD) control on the inverted pendulum and convince yourself that these policies cannot stabilize the system.*

*Try a PID control system and see how this might change how you can move the poles and zeros around. Does the added derivative control help that much?*

$$F(s) = K_p + \underline{K_d s} + \underline{K_i \frac{1}{s}}$$

